

Root Locus

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1 Review of related mathematics

1.1 Complex Algebra in Polar Form

For a complex number z , it can be expressed in polar form as

$$z = re^{j\theta}$$

Where $r = |z|$, $\theta = \tan^{-1} \frac{Im z}{Re z}$. Denote $r = |z|$ and $\theta = \angle z$

For multiple complex number

$$z_1 \times z_2 = |z_1| \angle z_1 \times |z_2| \angle z_2 = |z_1| |z_2| (\angle z_1 + \angle z_2)$$

$$z_1 \div z_2 = |z_1| \angle z_1 \div |z_2| \angle z_2 = \frac{|z_1|}{|z_2|} (\angle z_1 - \angle z_2)$$

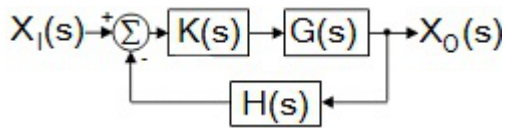
Similarly, for a function

$$z = \frac{\prod z_k}{\prod w_k} = \frac{(\prod |z_k|) (\sum \angle z_k)}{(\prod |w_k|) (\sum \angle w_k)} = \left(\frac{\prod |z_k|}{\prod |w_k|} \right) (\sum \angle z_k - \sum \angle w_k)$$

1.2 Roots of a equation

- Fundamental Theorem of Algebra : a order n polynomial equation has exactly n roots, including complex roots, equal roots, real roots.
- Complex roots occur in pairs
- If α is a double root of $f(x) = 0$, then it is also a root of $\frac{df(x)}{dx} = 0$

1.3 Review of transfer function



Consider a control system with plant $G(s)$, controller $K(s)$ and feedback $H(s)$, input $X_I(s)$ and output $X_O(s)$

- The open loop gain is $K(s)G(s)$
- The close loop gain is $\frac{K(s)G(s)}{1 + K(s)G(s)H(s)}$
- Then the characteristic equation of the close loop gain is $1 + K(s)G(s)H(s)$
- For simplicity, assume $K(s)$ is a number K
- The term $G(s)H(s)$ can be represented by a rational function $\frac{N(s)}{D(s)}$, and let the degree of $D(s)$ be n , and degree of $N(s)$ be m
- Let $G(s)H(s)$ has overall degree of p , so $p = n - m$. For proper fraction, $n \geq m$, i.e. $p \geq 0$
- By Fundamental Theorem of Algebra, and apply factorization, $G(s)H(s) = \frac{\sum_{k=1}^m b_k s^k}{\sum_{k=1}^n a_k s^k} = \frac{b_0 \prod_{k=1}^m (s - z_k)}{a_0 \prod_{k=1}^n (s - p_k)}$
- So the characteristic equation is $1 + KG(s)H(s) = 1 + K \frac{b_0 \prod_{k=1}^m (s - z_k)}{a_0 \prod_{k=1}^n (s - p_k)}$
- Assume $K, b_0, a_0 > 0$

2 The Root Locus

The close loop transfer function $\frac{K(s)G(s)H(s)}{1 + K(s)G(s)H(s)}$ contains the characteristic equation $1 + K(s)G(s)H(s)$

For $K(s) = K$

$$1 + KG(s)H(s) = 1 + K \frac{b_0 \prod_{k=1}^m (s - z_k)}{a_0 \prod_{k=1}^n (s - p_k)} = 1 + K \frac{b_0 (s - z_1)(s - z_2) \dots (s - z_m)}{a_0 (s - p_1)(s - p_2) \dots (s - p_n)} = 0$$

i.e.

$$K \frac{b_0 (s - z_1)(s - z_2) \dots (s - z_m)}{a_0 (s - p_1)(s - p_2) \dots (s - p_n)} = -1$$

It can be seen that, as K varies, poles will change, the locus of poles when K changes is the root locus.

As this is a complex variable function, so we can consider the equality of both magnitude and phase of this equation

$$KG(s)H(s) = K \frac{N(s)}{D(s)} = -1 \Rightarrow \begin{cases} \left| K \frac{N(s)}{D(s)} \right| = |-1| \\ \angle K \frac{N(s)}{D(s)} = \angle -1 \end{cases}$$

$$\therefore \begin{cases} K \in \mathbb{R}^+ \Rightarrow \angle K = 0^\circ \\ \angle -1 = 180^\circ + l \times 360^\circ \end{cases} \Rightarrow \begin{cases} K \left| \frac{N(s)}{D(s)} \right| = 1 \\ \angle \frac{N(s)}{D(s)} = 180^\circ + l \times 360^\circ \end{cases}$$

2.1 The Rules

2.1.1 Root locus is symmetric about real axis

The characteristic equation, $D(s) = 0$ has real coefficients, so its roots must occur in complex conjugate pairs that are symmetric about the real axis. And the root locus is a diagram of roots of the characteristic equation (or equivalently poles of $G(s)$), so it is also symmetric about the real axis.

2.1.2 Number of branches of root locus = order of characteristic equation (number of poles of $G(s)$)

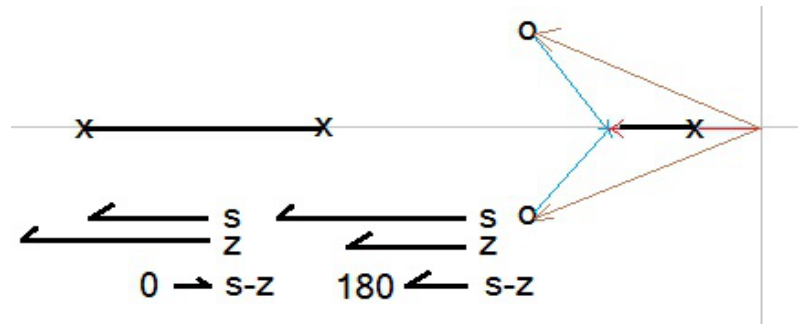
The root locus is the locus of poles as K varies, so the number of branches is the number of poles (order of characteristic equation), which is n .

2.1.3 Root locus starts at poles of $G(s)$, and ends at zeros of $G(s)$.

$K \left| \frac{N(s)}{D(s)} \right| = 1 \Rightarrow K |N(s)| = |D(s)|$, at the beginning, when $K = 0$, then $D(s) = 0$, i.e. the root locus starts at poles of the characteristic equation.

$K \left| \frac{N(s)}{D(s)} \right| = 1 \Rightarrow \left| \frac{N(s)}{D(s)} \right| = \frac{1}{K}$, at the end, when $K \rightarrow \infty$, then $N(s) = 0$, i.e. the root locus ends at zeros of the characteristic equation.

2.1.4 Segments on the real axis that have an odd number of poles and zeros to their left are part of the root locus



$$\text{Start with } \angle \frac{N(s)}{D(s)} = 180^\circ + l \times 360^\circ$$

$$\Leftrightarrow \angle N(s) - \angle D(s) = 180^\circ + l \times 360^\circ = k \times 180^\circ \quad k \text{ is odd}$$

$$\Leftrightarrow \sum \angle (s - z_k) - \sum \angle (s - p_k) = k \times 180^\circ$$

From the diagram, a z that is on the left of the s , its resultant $s - z$ has an angle of 0° .

From the diagram, a z that is on the right of the s , its resultant $s - z$ has an angle of 180° .

Using the same logic for poles, then

The term $\sum \angle (s - z_k) - \sum \angle (s - p_k)$ means the angle difference between all the zeros and poles, since any zero or pole on the left of the s result in 0° , so only consider the zero and pole on the right side of s .

Since one zero on the right side of s contributes to 180° and the same as the pole does. But since the angle $(s - p)$ is negative, so it means subtract 180° .

By the $\sum \angle (s - z_k) - \sum \angle (s - p_k) = k \times 180^\circ$, k is an odd number, then

Segments on the real axis that have an odd number of poles and zeros to their right are part of the root locus.

For poles and zeros not on the real axis, from the diagram, the angles cancel out by the conjugate pairs, so those are not counted.

2.1.5 The asymptotes as $s \rightarrow \infty$ is in $\alpha = \frac{\sum p_i - \sum z_i}{q}$, $\phi = \frac{180^\circ + l \cdot 360^\circ}{q}$

Consider the characterisitic eqaution

$$1 + KG(s)H(s) = 1 + K \frac{b_0 s^m + b_1 s^{m-1} + \dots + b_m}{a_0 s^n + a_1 s^{n-1} + \dots + a_n}$$

Take $\frac{s^m}{s^n}$ out

$$1 + KG(s)H(s) = 1 + K \frac{s^m}{s^n} \frac{b_0 + \frac{b_1}{s} + \dots + \frac{b_m}{s^m}}{a_0 + \frac{a_1}{s} + \dots + \frac{a_n}{s^n}} = 1 + K \frac{1}{s^{n-m}} \frac{b_0 + \frac{b_1}{s} + \dots + \frac{b_m}{s^m}}{a_0 + \frac{a_1}{s} + \dots + \frac{a_n}{s^n}} = 1 + \frac{K}{s^q} \frac{b_0 + \frac{b_1}{s} + \dots + \frac{b_m}{s^m}}{a_0 + \frac{a_1}{s} + \dots + \frac{a_n}{s^n}}$$

Thus

$$\lim_{s \rightarrow \infty} 1 + KG(s)H(s) = 1 + \frac{K b_0}{s^q a_0} = 1 + K \frac{b_0}{a_0} s^{-q}$$

Then consider the phase

$$\begin{aligned} \angle \left(\lim_{s \rightarrow \infty} 1 + KG(s)H(s) \right) &= \angle \left(\lim_{s \rightarrow \infty} 1 + KG(s)H(s) \right) \\ &= \angle \left(\lim_{s \rightarrow \infty} 1 + K \frac{N(s)}{D(s)} \right) \\ &= \angle \left(1 + K \frac{b_0}{a_0} s^{-q} \right) \\ &= \angle \left(1 + \underbrace{K \frac{b_0}{a_0}}_{\mathbb{R}^+} |s|^{-q} e^{jq\phi} \right) \end{aligned}$$

By $\angle \mathbb{R}^+$ can be ignore and $\angle \frac{N(s)}{D(s)} = 180^\circ + l \times 360^\circ$ and

$$\angle (e^{jq\phi}) = q\phi = 180^\circ + l \times 360^\circ$$

$$\therefore \phi = \frac{180^\circ + l \times 360^\circ}{q}$$

2.1.6 The breakaway / break in points

When more than one branches meet in the break-away / break-in point, that point is a multiple root of $1 + KG(s)H(s) = 0$

As the break-away / break-in point is a multiple root of $1 + KG(s)H(s) = 0$, so it is also a root of $\frac{d}{ds}KG(s)H(s) = 0$

Let the break away / break in point be x

$$1 + KG(x)H(x) = 0 \Rightarrow 1 + K\frac{N(x)}{D(x)} = 0 \Rightarrow \begin{cases} D(x) + KN(x) = 0 \\ D'(x) + KN'(x) = 0 \end{cases}$$

Eliminate the K

$$K = -\frac{D(x)}{N(x)} = -\frac{D'(x)}{N'(x)} \Rightarrow D(x)N'(x) = D'(x)N(x) \Rightarrow N'(x)D(x) - D'(x)N(x) = 0$$

Consider

$$\frac{d}{ds}G(s)H(s) = \frac{d}{ds}\frac{N(s)}{D(s)} = \frac{N'(s)D(s) - N(s)D'(s)}{D^2(s)}$$

Plug in the equation $N'(x)D(x) - D'(x)N(x) = 0$, so to find the break-in / break-away point is to solve

$$\frac{d}{ds}G(s)H(s) = 0$$

2.1.7 If the root locus crosses the stability boundary (the imaginary axis), the crossing point can be found by solving $1 + KG(j\omega)H(j\omega) = 0$

Recall that, the location of the poles of the system T.F. determine the damping property of the system.

For stable system, the poles is in LHP (Left Half Plane)

When the poles lies on the imaginary axis, (i.e. real part is zero), the system output is no-damped oscillation, it is the boundary case for stable system.

When the poles has positive real part $e^{pt} = e^{Re(p)t}e^{jIm(p)t} \rightarrow \infty$ as $t \uparrow$, so the system is unstable. So the boundary stable case can be found by solving

$$1 + KG(s)H(s) = 0 \quad s \text{ lies on imaginary axis}$$

i.e.

$$1 + KG(j\omega)H(j\omega) = 0$$

—END—