

Asymptotic Bode Plot & Lead-Lag Compensator

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1. Introduction

Consider a general transfer function

$$G(s) = \frac{\sum_{k=0}^n a_k s^k}{\sum_{k=0}^m b_k s^k} = A \frac{\prod_{k=0}^n (s - z_k)}{\prod_{k=0}^m (s - p_k)} \quad m > n$$

When $s = j\omega$, transfer function $G(j\omega)$ is very useful in frequency response analysis. As now the transfer function, or using another name, the *gain* is a function of frequency ω , it means that “amplification ability” of such system change as ω change, where the ω is the input or operating frequency.

There are some methods to investigate the behaviour of such “amplification ability changes”: Bode Plot, Nyquist Plot, Nichol Plot.

The *Bode Plot* consists of 2 plots: the magnitude plot and the phase plot, it is an *asymptotic* plot, an approximation plot.

The magnitude Bode Plot is $20\log|G(j\omega)|$ (y-axis) vs ω (x-axis, log scale)

The magnitude axis is expressed in dB of powers, it is a convention.

The frequency axis is expressed in log scale, it is also a convention, with a very good reason.

2. Review of some related mathematics

Log $\log \frac{AB}{CD} = \log A + \log B - \log C - \log D$ $\log \left| \frac{AB}{CD} \right| = \log |A| + \log |B| - \log |C| - \log |D|$

Standard Form $\log |j\omega + a| = \log \left| a \left(\frac{j\omega}{a} + 1 \right) \right| = \log |a| + \log \left| \frac{j\omega}{a} + 1 \right|$

Approximation Consider $\log \left| \frac{j\omega}{a} + 1 \right|$, a is called the *corner frequency*

$$\text{when } \begin{cases} \omega \ll a \\ \omega \gg a \end{cases} \Rightarrow \begin{cases} \frac{\omega}{a} \ll 1 \\ \frac{\omega}{a} \gg 1 \end{cases} \Rightarrow \begin{cases} \left| \frac{j\omega}{a} + 1 \right| \approx |1| = 1 \\ \left| \frac{j\omega}{a} + 1 \right| \approx \left| \frac{j\omega}{a} \right| = \frac{\omega}{a} \end{cases} \Rightarrow \begin{cases} \log \left| \frac{j\omega}{a} + 1 \right| \approx 0 \\ \log \left| \frac{j\omega}{a} + 1 \right| \approx \log \frac{\omega}{a} \end{cases}$$

$$\Leftrightarrow \begin{cases} 20 \log \left| \frac{j\omega}{a} + 1 \right| = 0 & \text{Flat horizontal line} \\ +20 \log \left| \frac{j\omega}{a} + 1 \right| = +20 \log \frac{\omega}{a} & \text{Stright line increasing with 20dB per decade} \end{cases}$$

Arc-Tan

$$\tan^{-1} \infty = \pm \frac{\pi}{2} \quad \tan^{-1} 0 = 0$$

3. Example

For example, consider a degree 1 transfer function with 5 zeros and poles.

$$G(s) = \frac{A(s+a)(s+b)}{(s+c)(s+d)(s+e)}$$

Where $-a$, $-b$ are zeros, $-c$, $-d$, $-e$ are poles.

Before doing the Bode Plot analysis, turn the transfer function into “Standard Form”

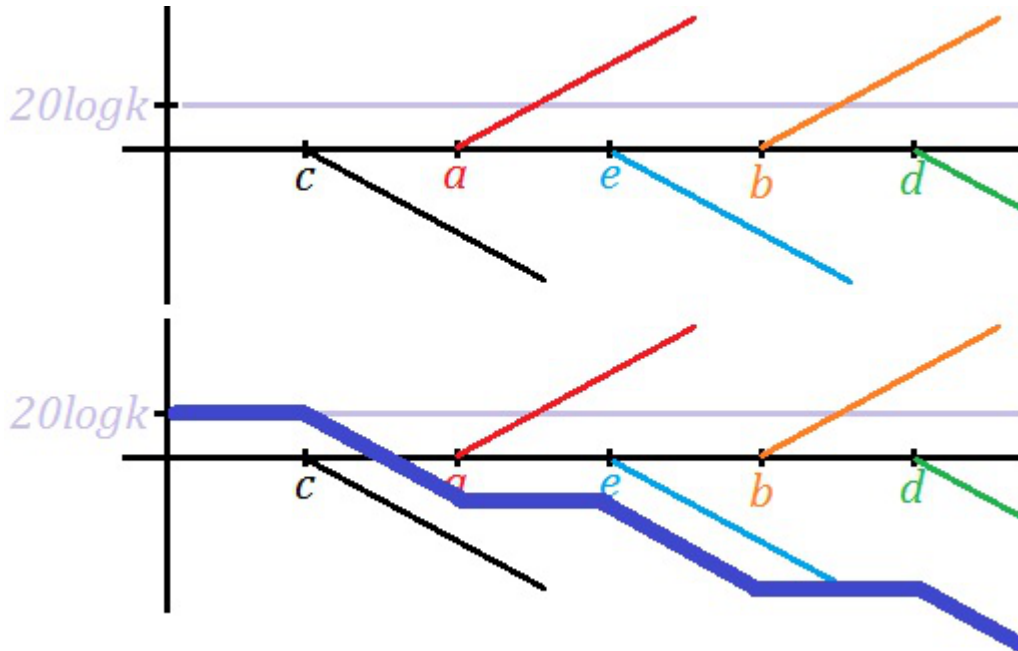
$$G(s) = \frac{Aab}{cde} \cdot \frac{\left(\frac{s}{a} + 1\right) \left(\frac{s}{b} + 1\right)}{\left(\frac{s}{c} + 1\right) \left(\frac{s}{d} + 1\right) \left(\frac{s}{e} + 1\right)} = \frac{k \left(\frac{s}{a} + 1\right) \left(\frac{s}{b} + 1\right)}{\left(\frac{s}{c} + 1\right) \left(\frac{s}{d} + 1\right) \left(\frac{s}{e} + 1\right)} \quad k = \frac{Aab}{cde}$$

The magnitude (in dB of powers) is thus

$$20 \log |G(s)| = 20 \log \left| \frac{k \left(\frac{s}{a} + 1\right) \left(\frac{s}{b} + 1\right)}{\left(\frac{s}{c} + 1\right) \left(\frac{s}{d} + 1\right) \left(\frac{s}{e} + 1\right)} \right|$$

$$= 20 \log |k| + 20 \log \left| \frac{s}{a} + 1 \right| + 20 \log \left| \frac{s}{b} + 1 \right| - 20 \log \left| \frac{s}{c} + 1 \right| - 20 \log \left| \frac{s}{d} + 1 \right| - 20 \log \left| \frac{s}{e} + 1 \right|$$

The Bode Plot is thus



4. For more general case

- The Effect of DC term : a horizontal line
- The Effect of a pole at α : For $\omega < \alpha$, no effect (since it is in log scale !), for $\omega > \alpha$, it goes down at a rate of 20dB per decade.
- The Effect of a zero at β : For $\omega < \beta$, no effect (since it is in log scale !), for $\omega > \beta$, it goes up at a rate of 20dB per decade.

More General

- For a *simple* , 1^{st} order pole at α : For $\omega < \alpha$, no effect, for $\omega > \alpha$, it goes down at a rate of $1 \cdot 20\text{dB}$ per decade.
- For a n^{th} order pole at β : For $\omega < \alpha$, no effect, for $\omega > \alpha$, it goes down at a rate of $n20$ dB per decade.
- In same logic, a m^{th} order zero at γ will give a increasing straight with slope of $m20\text{dB}$ per decade , starting at $\omega = \gamma$

5. Summary of Magnitude Plot

The algorithm to draw Magnitude Bode Plot is

- Turn the transfer function into standard form $(s + a) \rightarrow a(\frac{s}{a} + 1)$
- Find all the corner frequency
- For zeros, the lines go up. For poles, the lines go down.
- The slope of the line is $20\text{dB} \cdot \text{the degree of the pole/zero}$.

6. Phase Plot

Consider $(j\omega + a)$, the angle of this term is $\tan^{-1} \frac{\omega}{a}$

When $\omega \ll a$ (The axis is in scale of decade, i.e. 10 time)

$$\omega = 0.1a \quad \tan^{-1} \frac{\omega}{a} = \tan^{-1}(0.1) = 5.7^\circ$$

$$\omega = 0.01a \quad \tan^{-1} \frac{\omega}{a} = \tan^{-1}(0.01) = 0.57^\circ$$

When $\omega \gg a$ (The axis is a log scale, so consider a decade , i.e. 10 time)

$$\omega = 10a \quad \tan^{-1} \frac{\omega}{a} = \tan^{-1}(10) = 84.3^\circ$$

$$\omega = 100a \quad \tan^{-1} \frac{\omega}{a} = \tan^{-1}(100) = 89.4^\circ$$

So in general,

$$\tan^{-1} \frac{\omega}{a} \approx \begin{cases} 0^\circ & \omega \ll a \\ 90^\circ & \omega \gg a \end{cases}$$

7. Examples

$$G(s) = \frac{K_0}{T_0 s + 1} \quad K_0, T_0 > 0$$

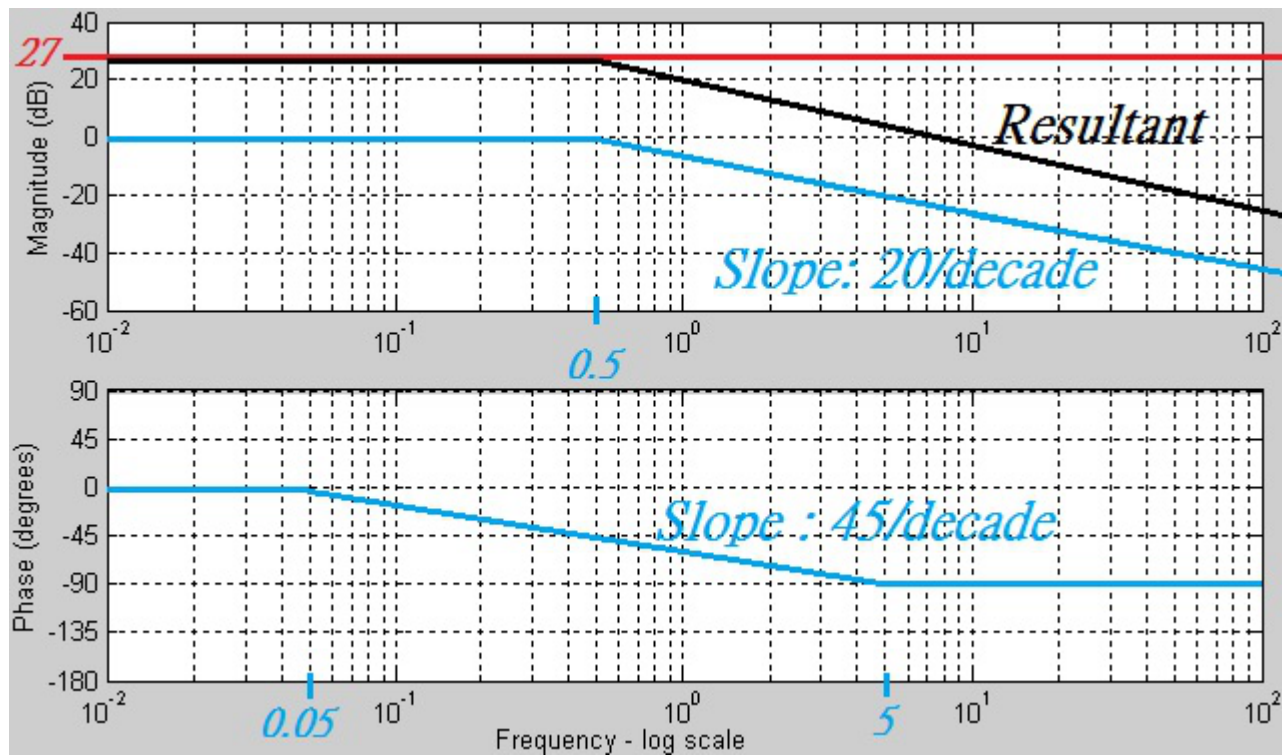
$$20 \log |G(j\omega)| = 20 \log |K_0| - 20 \log \left| \frac{j\omega}{1/T_0} + 1 \right|$$

$$\angle G(j\omega) = \underbrace{\angle K_0}_0 - \angle \left(\frac{j\omega}{1/T_0} + 1 \right)$$

Let $K = 4$, $T_0 = 0.5$

$$G(s) = \frac{4}{\frac{1}{2}s + 1}$$

- $20 \log |4| = 27$
- Corner Frequency in magnitude plot : 0.5
- Corner Frequency in phase plot : 0.05 and 5



8. Example 2

$$G(s) = \frac{K_0}{(s+a)(s+b)^2} \quad K_0, a, b > 0$$

First change it into standard form

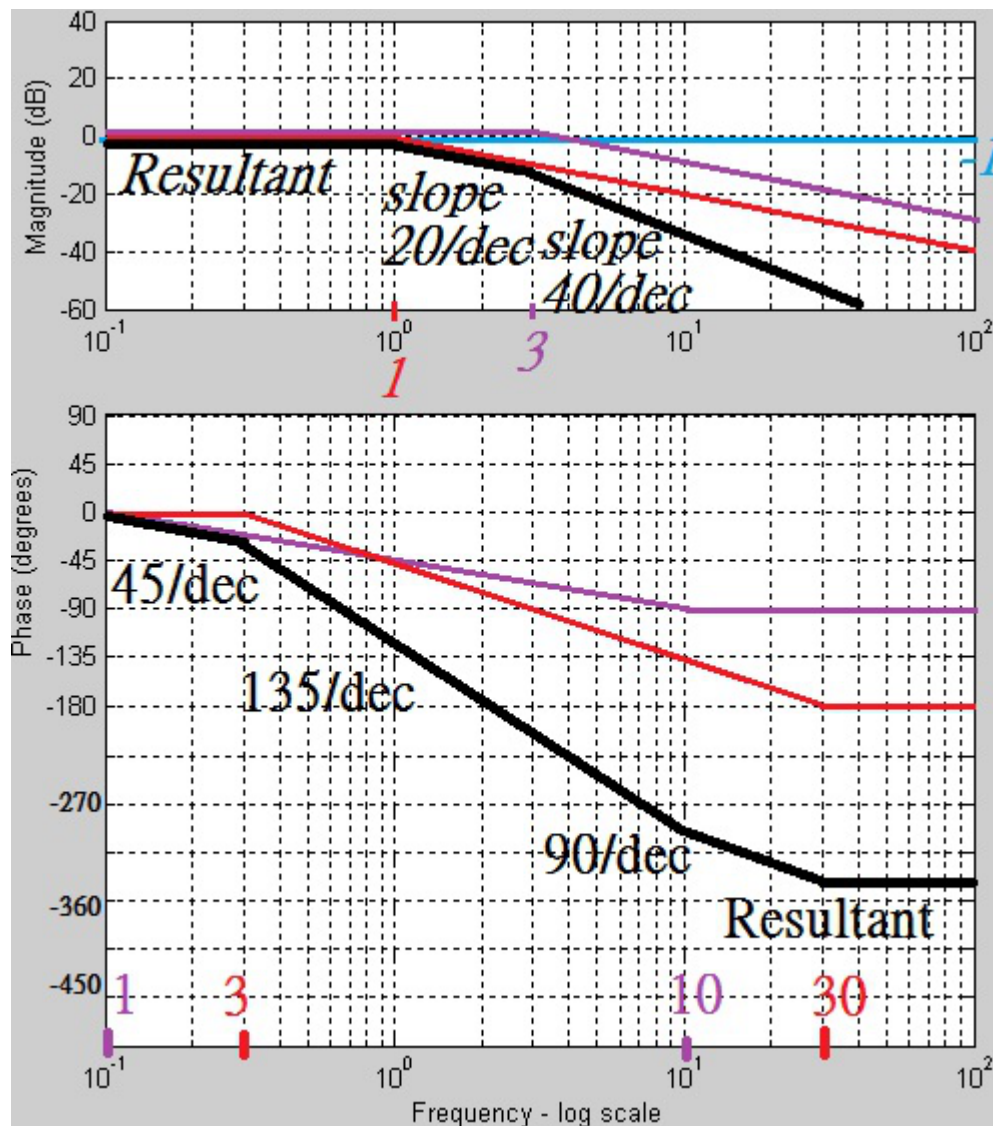
$$G(s) = \frac{\frac{K_0}{ab^2}}{\left(\frac{s}{a} + 1\right) \left(\frac{s}{b} + 1\right)^2}$$

$$20 \log |G(j\omega)| = 20 \log \left| \frac{K_0}{ab^2} \right| - 20 \log \left| \frac{j\omega}{a} + 1 \right| - 2 \times 20 \log \left| \frac{j\omega}{b} + 1 \right|$$

$$\angle G(j\omega) = \underbrace{\angle \left(\frac{K_0}{ab^2} \right)}_0 - \angle \left(\frac{j\omega}{a} + 1 \right) - 2 \angle \left(\frac{j\omega}{b} + 1 \right)$$

Let $K_0 = 8$, $a = 1$, $b = 3$

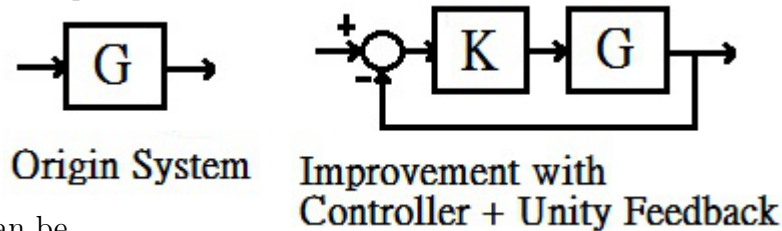
- $20 \log \left| \frac{8}{9} \right| = -1$
- Corner Frequency in magnitude plot : 1 , 3
- Corner Frequency in phase plot : 0.1 & 10 , 0.3 & 30



9. Lead Lag Compensator $\frac{1 + Ts}{1 + \alpha Ts}$

Purpose of Compensator

System is not always perfect naturally, some improvements can be made by adding a special type of controller, the Lead-Lag Compensator



The improvements can be

- Increase Gain
- Reduce steady state Error
- Force the system response faster
- Force the system become less oscillatory
- Increase bandwidth
- Improve stability margin

The Lead and the Lag Compensator

There are two form, both are the same

$$\frac{1 + \alpha Ts}{1 + Ts} \quad \text{or} \quad \frac{1 + Ts}{1 + \alpha Ts}$$

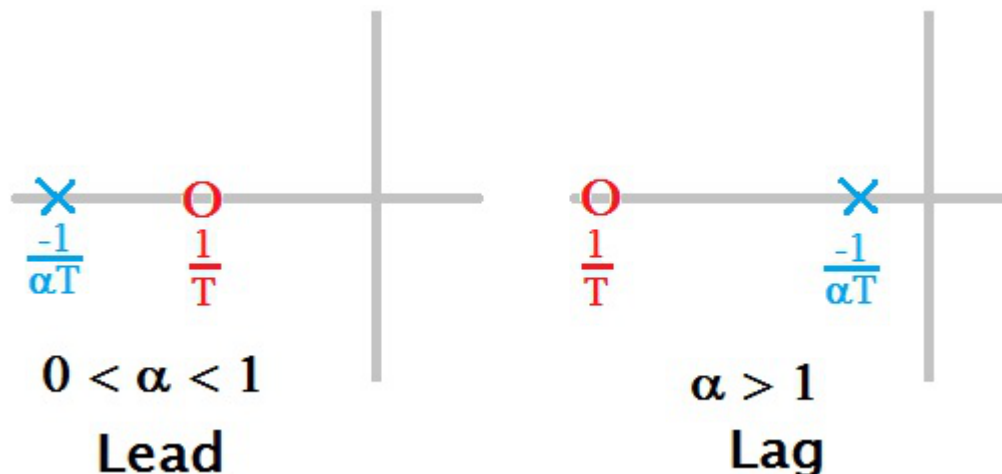
Consider the second one

$$K_{DC} \frac{1 + Ts}{1 + \alpha Ts}$$

K_{DC} : DC gain , when $G(s)_{s=0}$

The Transfer Function of the compensator has 1 zero and 1 poles : $\frac{-1}{T}$ and $\frac{-1}{\alpha T}$

The α is key parameter here.



Consider their Bode Plot

$$K(s) = K_{DC} \frac{1 + Ts}{1 + \alpha Ts}$$

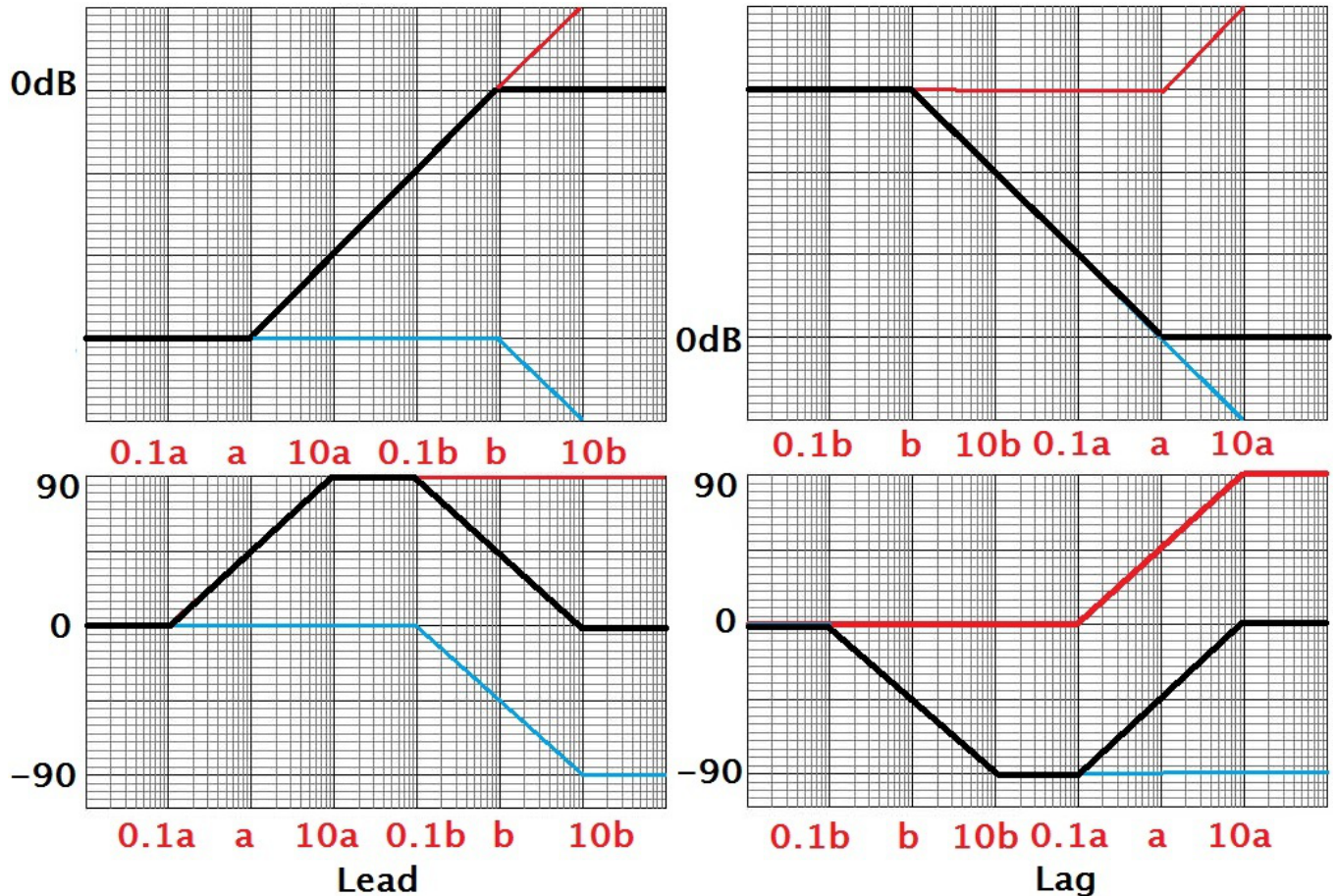
Standard Form

$$K(s) = K_{DC} \frac{1 + \frac{s}{1/T}}{1 + \frac{s}{1/\alpha T}}$$

$$20 \log |K(j\omega)| = 20 \log |K_{DC}| + 20 \log \left| 1 + j \frac{\omega}{1/T} \right| - 20 \log \left| 1 + j \frac{\omega}{1/\alpha T} \right|$$

$$\angle K(j\omega) = \underbrace{\angle K_{DC}}_0 + \angle \left(1 + j \frac{\omega}{1/T} \right) - \angle \left(1 + j \frac{\omega}{1/\alpha T} \right)$$

- Corner frequency of magnitude plot : $\frac{1}{T}$, $\frac{1}{\alpha T}$
- Corner frequency of phase plot : $\frac{1}{10T}$ & $\frac{10}{T}$ and $\frac{1}{10\alpha T}$ & $\frac{10}{\alpha T}$
- Denote $\frac{1}{T} = a$ $\frac{1}{\alpha T} = b$
- The following Bode Plot ignore the DC part (Assume $K_{DC} = 1$)



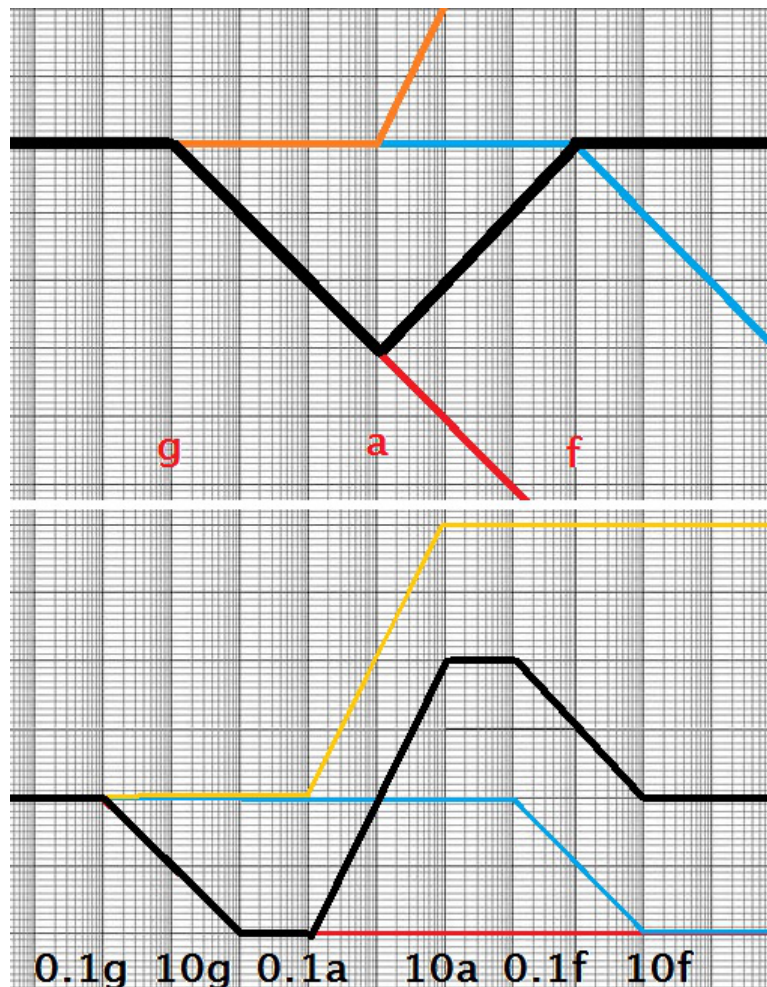
Lead-Lag compensator

$$K(s) = K_{DC} \cdot \frac{1 + Ts}{1 + \alpha_1 Ts} \cdot \frac{1 + Ts}{1 + \alpha_2 Ts}$$

$$20 \log |K| = 20 \log |K_{DC}| + 2 \times 20 \log \left| 1 + j \frac{\omega}{1/T} \right| - 20 \log \left| 1 + j \frac{\omega}{1/\alpha_1 T} \right| - 20 \log \left| 1 + j \frac{\omega}{1/\alpha_2 T} \right|$$

$$\angle K = 2\angle \left(1 + j \frac{\omega}{1/T} \right) - \angle \left(1 + j \frac{\omega}{1/\alpha_1 T} \right) - \angle \left(1 + j \frac{\omega}{1/\alpha_2 T} \right)$$

- Corner frequency in magnitude plot : $\frac{1}{T}$ (denote as a) , $\frac{1}{\alpha_1 T}$ denote as f , $\frac{1}{\alpha_2 T}$ denote as g
- $g < a < f$
- Corner frequency in phase plot : $0.1a, 10a$, $0.1f, 10f$, $0.1g, 10g$



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